AMENDMENT TO THE CLAIMS:

This listing of claims will replace all prior versions, and listings, of claims in the application:

Claim 1 (currently amended): A method of manufacturing strained billets from metal chips, comprising the steps of:

crushing said chips into particles;

cleaning said particles;

cold molding of said particles into cylindrical shape briquettes;

placing said briquettes into a capsule;

sealing sealing in said capsule with upper and lower buttend covers;

heating said capsule to a temperature in the range of 900 - 1080 deg C, and maintaining it at this temperature for a time sufficient for temperature equalization throughout the capsule volume;

loading said capsule into the mould section of a pressing rig, said pressing rig further having an upper plunger with a principal press-washer and a lower plunger with an autonomous press washer each plunger extending into said mould section on opposite ends of said capsule; hot deforming said capsule in the axial direction, wherein said hot deformation deforming is carried out by application of dynamic impingement force by said press washers uniformly applied over the surfaces of said capsule butt-end covers, with sufficient repetitions and magnitude of force to result in a billet having the desired relative density;

and then subsequent cooling of said formed billet.

- Claim 2 (currently amended): The method in accordance with claim

 1, wherein said <u>particles have</u> <u>particles!</u> sizes <u>are</u> in the range of 5 -20 mm.
- Claim 3 (currently amended): The method of claim 1 wherein said metal is selected consisting of a titanium alloy alloys.
- Claim 4 (currently amended): The method of claim 1 wherein said pressing rig is preheated to a temperature not less than 0.2 that of the capsule temperature prior to placement of said capsule in said pressing rig. [;]
- Claim 5 (original): The method of claim 1 wherein:

 at least one of said butt-end covers has a diameter

 (reduced diameter) less than the capsule diameter by two

 thicknesses of the capsule cowling;

 wherein the diameter of said press-washer (reduced

 diameter) adjacent to said reduced diameter butt-end cover

 is also less than the capsule diameter by two thicknesses

 of the capsule cowling; and

 wherein said reduced diameter press-washer in cooperation

 with said mould section forms a chamber to receive capsule

 cowling shed during said hot deforming step.
- Claim 6 (currently amended): The method of claim 5 wherein:

 the sum of each said chamber volume and change in volume
 experienced by said capsule during hot deforming

 deformation define defines a work space; and

- wherein the height of said work space is defined by: N x $(H_1 H_2)$, where N is <u>selected chosen from in</u> the range consisting of 1.2 1.5, and H_1 and H_2 are the capsule preand post- hot deformation axial dimensions.
- Claim 7 (currently amended): The method of claim 1 wherein said cleaning step comprises the steps of: rinsing, drying and magnetic separating separation.
- Claim 8 (currently amended): The method of claim 1 wherein:

 said cleaned particles are further subjected to vacuum
 thermal degassing (VTD), said VTD comprising the steps of:
 heating said particles to a temperature in the range of 550
 650 deg C under a vacuum pressure of 5 x 10 3 5 x 10 3 mm
 Hg,
 maintaining said particles at said temperature and pressure
 for a time duration of about 1 to 2 hours,
 cooling said particles down to about 200 deg C at said
 vacuum pressure,
 and cooling said particles to ambient pressure and
 temperature.
- Claim 9 (original): The method of claim 1, wherein said cold molding step results in briquettes having relative density of at least 0.6.
- Claim 10 (currently amended): The method of claim 1, wherein said hot <u>deforming deformation</u> step results in a deformation degree value of capsule deformation of at least 35%.

- Claim 11 (currently amended): The method of claim 1, wherein said hot <u>deforming deformation</u> step results in a billet relative density of at least 0.95.
- Claim 12 (currently amended): The method of claim 1, wherein said hot deforming deformation temperature is in the range of 900 1050 deg C.

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Claim 13 (cancelled):
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Claim 14 (cancelled):

Claim 15 (cancelled):